

## Centre d'usinage S axes

(1)  $\overrightarrow{O_3 O_5} = \overrightarrow{O_3 O_4} + \overrightarrow{O_4 O} + \overrightarrow{O O_5}$

$$= \vec{y} \cdot \vec{y}_3 + l_3 \cdot \vec{z}_3 + l_4 \cdot \vec{u}_4 + z \cdot \vec{z}_5$$

$$= l_4 \cdot \vec{u}_3 + \vec{y} \cdot \vec{y}_3 + (l_3 + z) \cdot \vec{z}_3$$

(2) Par dérivation :  $\dot{J}_{O_5 E_6/3} = \left[ \frac{d \overrightarrow{O_3 O_5}}{dt} \right]_3$

$$= \overset{\circ}{y} \cdot \overset{\circ}{y}_3 + \overset{\circ}{z} \cdot \overset{\circ}{z}_3$$

compositus des vitess:  $\dot{J}_{O_5 E_6/3} = \dot{J}_{O_5 E_6/5} + \dot{J}_{O_5 E_5/4} + \dot{J}_{O_5 E_4/3}$

Où:  $\dot{J}_{O_5 E_6/5} = \vec{0}$  car  $O_5$  est sur l'axe de la pivot entre 6 et 5.

$\bullet \dot{J}_{O_5 E_5/4} = \overset{\circ}{z} \cdot \vec{z}_3$  (glissement)

$\bullet \dot{J}_{O_5 E_4/3} = \overset{\circ}{y} \cdot \vec{y}_3$  ("")

donc  $\dot{J}_{O_5 E_6/3} = \overset{\circ}{y} \cdot \vec{y}_3 + \overset{\circ}{z} \cdot \vec{z}_3$

(3.)  $\ddot{J}_{O_0 E_0/3} = \ddot{J}_{O_0 E_0/1} + \ddot{J}_{O_0 E_1/2} + \ddot{J}_{O_0 E_2/3}$

$\bullet \ddot{J}_{O_0 E_0/1} = \vec{0} = -l_0 \cdot \vec{u}_1$

$\bullet \ddot{J}_{O_0 E_1/2} = \ddot{J}_{O_0 E_1/2} + \overrightarrow{O_0 O_1} \wedge \overrightarrow{I_{1/2}} = \theta_1 \cdot \vec{y}_1$

$$\text{B } \vec{J}_{0,\epsilon_{2/3}} = \vec{v} \cdot \vec{u}_3$$

donc  $\boxed{\vec{J}_{0,\epsilon_{2/3}} = b_0 \cdot \dot{\theta}_1 \cdot \vec{u}_1 + \vec{v} \cdot \vec{u}_3}$

4.  $v_{\eta} = \vec{J}_{\eta \epsilon_{0/3}} \cdot \vec{q}_3$

$$= \vec{J}_{\eta \epsilon_{0/1}} \cdot \vec{q}_3 + \vec{J}_{\eta \epsilon_{1/2}} \cdot \vec{q}_3 + \vec{J}_{\eta \epsilon_{2/3}} \cdot \vec{q}_3$$

$$\bullet \vec{J}_{\eta \epsilon_{0/1}} \cdot \vec{q}_3 = \cancel{\vec{J}_{\eta \epsilon_{0/1}}} \cdot \vec{q}_3 + (\vec{r}_{00} \times \vec{r}_{0/1}) \cdot \vec{q}_3$$

et  $\vec{r}_{00} = \vec{u}_0 \cdot \vec{u}_0 + \vec{v}_0 \cdot \vec{v}_0 + \vec{w}_0 \cdot \vec{w}_0$

$$\begin{aligned} \vec{J}_{\eta \epsilon_{0/1}} \cdot \vec{q}_3 &= - \left( [u_0 \cdot \vec{u}_0 + v_0 \cdot \vec{v}_0 + w_0 \cdot \vec{w}_0] \times (\dot{\theta}_0 \cdot \vec{z}_{01}) \right) \cdot \vec{q}_3 \\ &= - (-u_0 \cdot \vec{q}_0 + v_0 \cdot \vec{w}_0) \cdot \dot{\theta}_0 \cdot \vec{q}_3 \\ &= (u_0 \cdot \cos \theta_0 - v_0 \cdot \sin \theta_0) \cdot \dot{\theta}_0. \end{aligned}$$

$$\bullet \vec{J}_{\eta \epsilon_{1/2}} \cdot \vec{q}_3 = \cancel{\vec{J}_{0,\epsilon_{1/2}}} \cdot \vec{q}_3 + (\vec{r}_{01} \times \vec{r}_{1/2}) \cdot \vec{q}_3 \stackrel{=\dot{\theta}_1 \cdot \vec{q}_3 \text{ car } \vec{r}_{01} \parallel \vec{r}_{1/2}}{\text{annule}} = 0$$

$$\bullet \vec{J}_{\eta \epsilon_{2/3}} \cdot \vec{q}_3 = \vec{v} \cdot \vec{u}_3 \cdot \vec{q}_3 = 0$$

Donc:  $\boxed{\vec{J}_{\eta \epsilon_{0/3}} \cdot \vec{q}_3 = v_{\eta} = (u_0 \cdot \cos \theta_0 - v_0 \cdot \sin \theta_0) \cdot \dot{\theta}_0}$

5. On écrit  $\vec{J}_{\eta \epsilon_{0/3}} \rightarrow \vec{J}_{\eta \epsilon_{0/1}} = \vec{u}_0$ , il faut donc:

$$\vec{J}_{\eta \epsilon_{0/3}} + \vec{J}_{\eta \epsilon_{3/2}} = \vec{u}_0$$

$$\vec{J}_{\eta \epsilon_{0/3}} = -\vec{J}_{\eta \epsilon_{3/2}} + \vec{u}_0 = \vec{J}_{\eta \epsilon_{0/3}} + \vec{u}_0$$

Et  $\vec{J}_{\text{vect}} = \vec{J}_{\text{vect}_3} = \dot{\vec{y}} \cdot \vec{\eta} + \dot{\vec{z}} \cdot \vec{z}$  (en usinage  $M = Os$ ).

Il faut donc :

$$0 = \dot{v}_{x\eta} + v_{ux}$$

$$\dot{y} = \dot{v}_{y\eta} + v_{uy}$$

$$\dot{z} = \dot{v}_{z\eta} + v_{uz}$$

Où  $\vec{v}_\eta = \begin{pmatrix} v_{ux} \\ v_{uy} \\ v_{uz} \end{pmatrix}$  ( $\vec{u}_3, \vec{\eta}_3, \vec{z}_3$ )

la vitesse d'usinage constante.