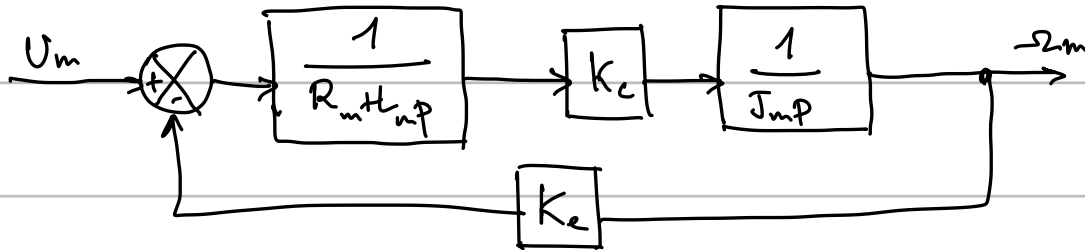


Correction du DS 4 SII MP&I PC&I

Q1: $U_m - E_m = R_m I_m + L_m p I_m \quad E_m = K_e \Omega_m$

$C_m = K_e I_m \quad J_m p \Omega_m = C_m$

Q2:



Q3: $H(p) = \frac{\Omega_m}{U_m} = \frac{\frac{K_e}{J_m p (R_m + L_m p)}}{1 + \frac{K_e K_c}{J_m p (R_m + L_m p)}}$

$$H(p) = \frac{1/K_e}{1 + \frac{J_m R_m}{K_e K_c} p + \frac{J_m L_m}{K_e K_c} p^2}$$

Q4: $K = \frac{1}{K_e} \quad \omega_0 = \sqrt{\frac{K_e K_c}{J_m L_m}} \quad z = \frac{1}{2} \omega_0 \times \frac{J_m R_m}{K_e K_c}$

$$z = \frac{1}{2} \sqrt{\frac{K_e K_c}{J_m L_m}} \times \frac{J_m^2 R_m^2}{K_e^2 K_c^2} = \frac{1}{2} \sqrt{\frac{J_m R_m^2}{L_m K_e K_c}} = z$$

Q5: $\tau_e = \frac{L_m}{R_m} \quad \text{et} \quad \tau_m = \frac{R_m J_m}{K_e K_c}$

on a $(1 + \tau_e p)(1 + \tau_m p) = 1 + (\tau_e + \tau_m)p + \tau_e \tau_m p^2$

Ce qui donne $1 + \underbrace{z_m \left(1 + \frac{z_c}{z_m}\right)}_{\approx z_m} p + \frac{L_m}{R_m} \times \frac{R_m J_m}{K_e K_c} p^2$

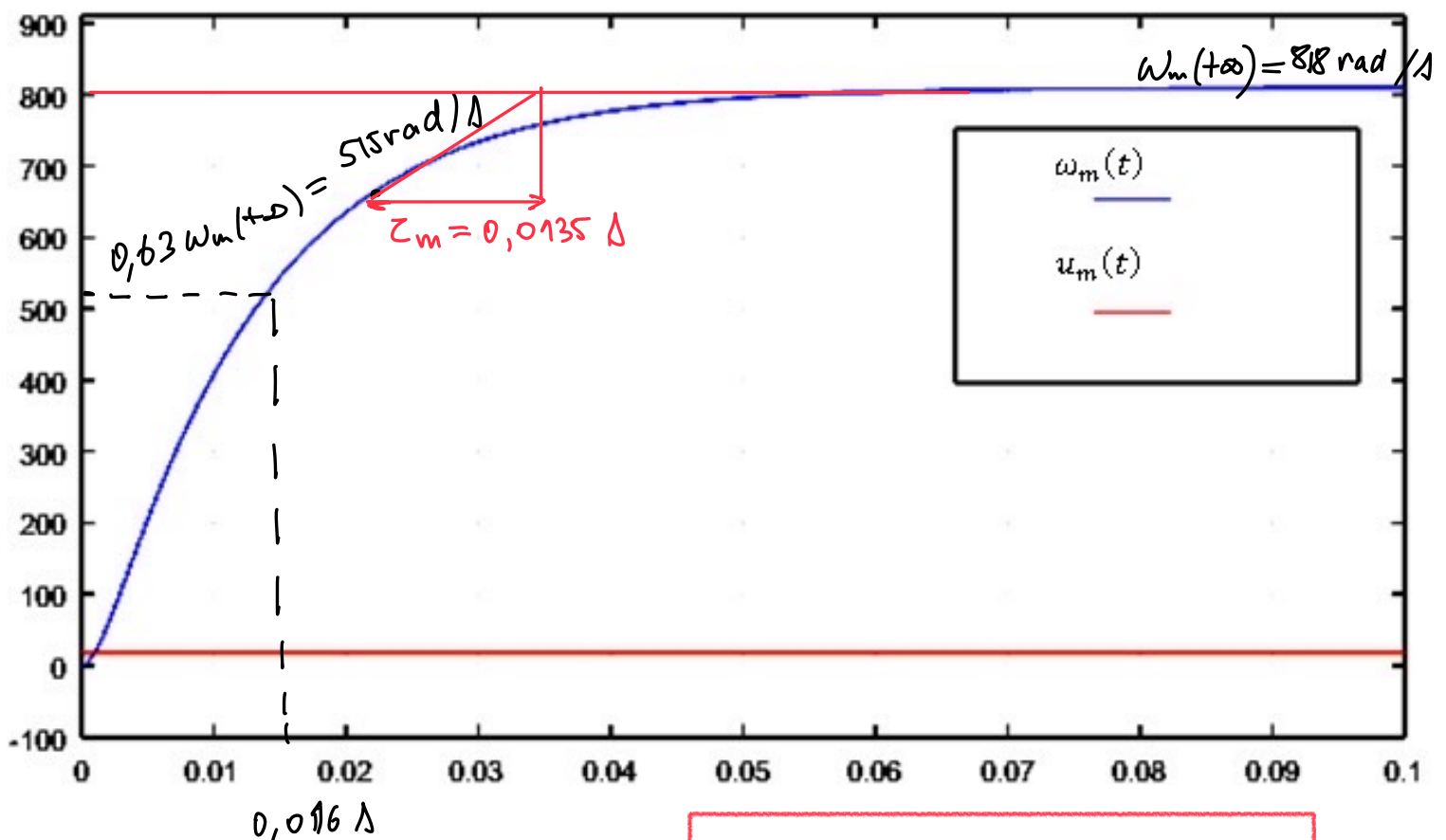
$$1 + \frac{J_m R_m}{K_e K_c} p + \frac{L_m J_m}{K_e K_c} p^2$$

on retrouve bien le dénominateur trouvé à la question Q3.

Q6: $\lim_{t \rightarrow \infty} \omega_m = \lim_{p \rightarrow 0} p \Omega(p) = \lim_{p \rightarrow 0} \cancel{p} \times \frac{18}{\cancel{p}} \times \frac{K}{(1+z_c p)(1+z_m p)} = 18 K$

A.N. $\omega(t \rightarrow \infty) = 18 \times \frac{1}{0,022} = 818 \text{ rad/s}$

Q7:



$$z_m = 0,0135 \text{ s}$$

on a $z_m + z_c = 0,016 \text{ s} \Rightarrow$

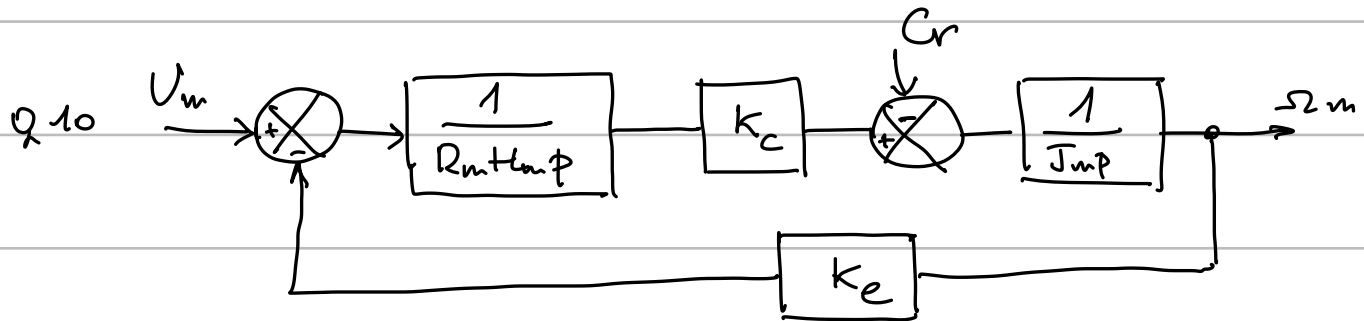
$$z_c = 0,016 - 0,0135 = 0,0025 \text{ s}$$

Q8: On peut approximer $H(p)$ à une fonction de transfert du premier ordre avec un retard de z_e

$$H(p) = \frac{K}{1 + z_m p}$$

Q9:

Sur le graphe on a une vitesse en régime permanent qui est égale à $\frac{810}{45 \times 18} \text{ rad/s} = \frac{810}{2\pi} \times 60 = \underline{7734 \text{ tr/min}} < 8000 \text{ tr/min}$



Q11 $F_1(p) = \left. \frac{\Omega_m}{U_m} \right|_{C_r=0} = H(p)$ $F_2(p) = \left. \frac{\Omega_m}{C_r} \right|_{U_m=0}$

$$F_2(p) = \frac{-\frac{1}{J_m p}}{1 + \frac{K_e K_c}{R_m + L_m p} \times \frac{1}{J_m p}} = \frac{-R_m + L_m p}{(J_m p)(R_m + L_m p) + K_e K_c}$$

Q12: On a d'après le schéma bloc:

$$\begin{aligned} \Omega_m(p) &= F(p) (B(p)U(p) - C_r(p)) \\ &= F(p)B(p)U(p) - F(p)C_r(p) \end{aligned}$$

$$\Rightarrow F(p)B(p) = H(p) \quad F(p) = -F_2(p)$$

Q13: Pour la modélisation figure 10

$$\lim_{t \rightarrow \infty} w_m(t) = \lim_{p \rightarrow 0} p \Omega_m(p) = \lim_{p \rightarrow 0} p \times \frac{1}{p} \times \frac{\cancel{k} \cancel{k_2} h}{\cancel{k_2} k_{2I} f} = \frac{k}{k_{2I} f}$$

Pour la modélisation figure 11:

$$\text{pour } C_v \rightarrow 0 \quad \lim_{t \rightarrow \infty} w_m(t) = \lim_{p \rightarrow 0} p \Omega_m(p) = \lim_{p \rightarrow 0} p \times \frac{1}{p} \times \frac{K}{k_{2I} (T_p + f)} = \frac{K}{k_{2I} f}$$

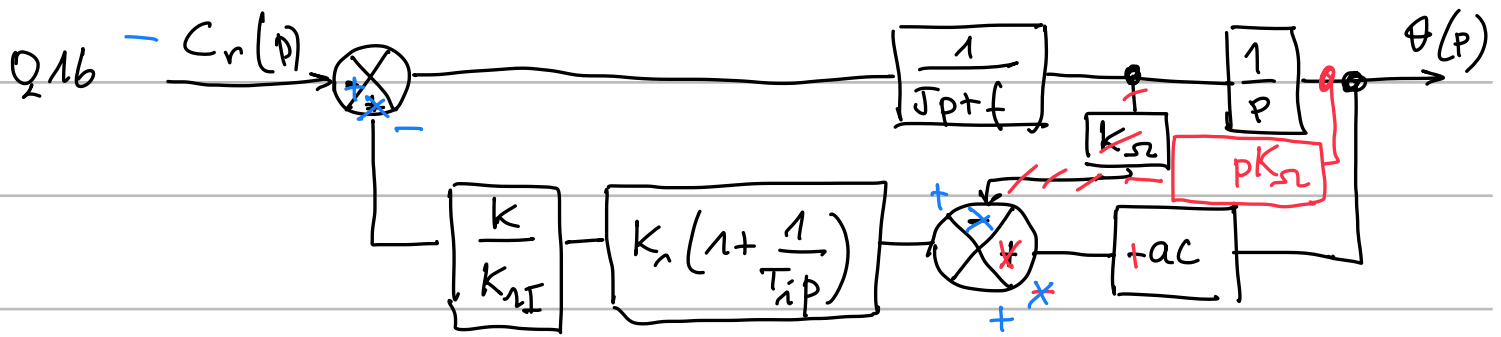
on peut dire que du point de vue du régime permanent la simplification est valide puisque la valeur finale est la même.

$$Q14: \frac{\Omega}{U_{cr}} = \frac{\frac{k_1 k}{k_{2I}} \times \frac{1}{(T_p + f)} \times \left(\frac{T_{1p} + 1}{T_{1p}} \right)}{1 + \frac{k_2 k_1 k}{k_{2I}} \times \frac{1}{(T_p + f)} \times \frac{T_{1p} + 1}{T_{1p}}} = \frac{K K_1 (T_{1p} + 1)}{k_{2I} (T_p + f) T_{1p} + K_2 K_1 K (T_{1p} + 1)}$$

$$Q15 \quad T_1 = \frac{J}{f} \quad H_\Omega(p) = \frac{K K_1 \left(\frac{J}{f} p + 1 \right)}{k_{2I} (T_p + f) \frac{J}{f} p + K_2 K_1 K \left(\frac{J}{f} p + 1 \right)}$$

$$H_\Omega(p) = \frac{K K_1}{J K_{2I} p + K_2 K_1 K} = \frac{1/k_2}{1 + \frac{J K_{2I}}{K_2 K_1 K} p}$$

$$b = \frac{1}{k_2} \quad ; \quad z = \frac{J K_{2I}}{K_2 K_1 K}$$



Modifications en rouge: puis modification en bleu

$$\text{d'où } \frac{\theta(p)}{C_r(p)} = \frac{\frac{1}{p} \left(\frac{1}{Tp+f} \right)}{1 + \frac{1}{p} \left(\frac{1}{Tp+f} \right) \frac{kk_n}{K_{nI}} \left(\frac{T_i p + 1}{T_i p} \right) (ac + pK_{\omega})}$$

$$\text{d'où } \frac{\theta(p)}{C_r(p)} = \frac{-K_{nI} T_i p}{K_{nI} T_i p^2 (Tp+f) + K k_n (T_i p + 1) (ac + pK_{\omega})} =$$

Pour un échelon unitaire $C_r(p) = \frac{1}{p}$

$$\text{donc } \lim_{t \rightarrow +\infty} \theta(t) = \lim_{p \rightarrow 0} p \theta(p) = \lim_{p \rightarrow 0} p \times \frac{1}{p} \times H_C(p) = 0$$

le correcteur rend le système insensible à la perturbation

$$Q17: \theta \dot{=} \frac{b}{p(zp+1)} (dp\theta_c + a(c\theta_c - c\theta))$$

$$\theta \left(1 + \frac{bac}{p(zp+1)} \right) = \theta_c (dp+ac) \times \frac{b}{p(zp+1)}$$

$$\frac{\theta}{\theta_c} = \frac{(dp+ac)b}{p(zp+1) + abc}$$

$$Q18: \mu = \theta_c - \theta = \theta_c \left(1 - \frac{(dp+ac)b}{p(z_{p+1})+abc} \right)$$

$$= \theta_c \left(\frac{p(z_{p+1})+abc - (dp+ac)b}{p(z_{p+1})+abc} \right)$$

$$= \theta_c \left(\frac{\cancel{p(z_{p+1})+abc} - dp - \cancel{abc}}{p(z_{p+1})+abc} \right)$$

$$\mu = \theta_c \left(\frac{p(z_{p+1}) - d}{p(z_{p+1})+abc} \right)$$

$$\mu_p = \lim_{p \rightarrow 0} \cancel{p} \times \frac{1}{\cancel{p}} \times \frac{p(z_{p+1}) - d}{p(z_{p+1})+abc} = 0$$

$$\mu_v = \lim_{p \rightarrow 0} \cancel{p} \times \frac{1}{\cancel{p^2}} \times \cancel{p} \left(\frac{z_{p+1} - d}{p(z_{p+1})+abc} \right) = \frac{1-d}{abc}$$

$$Q19: \mu_v = 0 \Rightarrow d = 1$$